

Figure 28. Distribution of water-budget components among the layers of the digital flow model for the Arnold Air Force Base area.

→ DIRECTION OF FLOW

Ground-Water Withdrawal Wells Particle Tracking

Currently (2005), ground-water withdrawal wells are operating at SWMU 1&2, SWMU 5, SWMU 8, and SWMU 10. Particle-tracking results from these SWMUs under conditions with the ground-water withdrawal wells pumping show that no particles leave the SWMUs (fig. 32).

In 2005, five new ground-water withdrawal wells along the airfield road were scheduled to begin pumping. To analyze the effect of these new wells on the flowpaths from SWMU 1&2, a particle-tracking simulation was performed with the existing ground-water withdrawal wells at SWMU 1&2 turned off and the new wells along the airfield road turned on. The airfield road ground-water withdrawal wells and the J4 test cell capture about 89 percent of the

particles from SWMU 1&2, with about 11 percent of the particles discharging near Rutledge Falls (fig. 33). To estimate the travel time of ground water from the area near the airfield road ground-water withdrawal wells to Big Spring at Rutledge Falls, a simulation was performed starting particles just downgradient of the capture area of the airfield road withdrawal wells. The estimate of travel time from the airfield road withdrawal wells area to Big Spring at Rutledge Falls ranges from 1 to 5 years with a mean travel time of 2 years and a median travel time of 2 years. This mean travel time of 2 years from the airfield road area to Big Spring at Rutledge Falls, compared with the mean travel time of 46 years from SWMU 1&2 to Big Spring at Rutledge Falls implies that the airfield road withdrawal wells should substantially reduce the time required to observe a change in contaminant discharge from the "northwest plume" at Big Spring at Rutledge Falls.

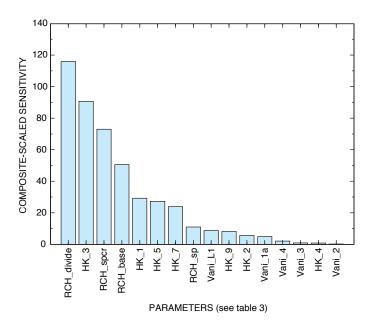


Figure 29. Composite-scaled sensitivities for model parameters.

Dewatering Facilities Particle Tracking

Three particle-tracking simulations were run to analyze the effects of dewatering facilities on flow paths in the Main Test Area (MTA). In the first simulation, particles were placed in the MTA (in a rectangular area bounded by Third and Fifth Streets and Avenues C and E) and tracked forward under conditions with all dewatering facilities turned on (fig. 34). In the second simulation, particles were placed in the MTA and tracked forward under conditions with all dewatering facilities turned off (fig. 35). In the third simulation, particles were placed at the location of the dewatering facilities and tracked backwards to their recharge locations (fig. 36). These simulations illustrate that the dewatering facilities have a substantial effect on flow paths that were simulated from the MTA and are effective in containing most of the ground water in this area.

Model Limitations

Models, by their very nature, are simplifications of the natural system. Factors that affect how well a model represents the natural system include the model scale; inaccuracies in estimating hydraulic properties; inaccurate or poorly defined boundary conditions; and the accuracy of pumping, water-level, and streamflow data. The model presented in this report is consistent with the conceptual model and hydrologic data of the area. The model uses a variably spaced grid so the model resolution is greatest near SWMUs, ground-water withdrawal

wells, and dewatering facilities. The model will not provide accurate predictions on a scale smaller than the grid resolution.

The hydraulic-conductivity zones used in the model represent large-scale variations in hydraulic properties; the actual spatial variations of hydraulic properties of the aquifer system occur on a much smaller scale and are poorly defined. Additionally, the aquifer system, being karst in nature, has a wide range of measured hydraulic conductivity. Finally, evidence indicates that the aquifer system behaves anisotropically, but no measured values of the degree of anisotropy exist.

The model is calibrated to average annual conditions during 2002 and may not represent flow during seasonal extremes. Seasonal potentiometric maps (Robinson and others, 2005) and continuous water-level data (fig. 16) indicate some local seasonal shifts in flow directions in the upper part of the Crumpton Creek Basin. Similarly, ground-water gradients near the divide north of SWMU 10 may change seasonally.

The particle-tracking program, MODPATH, is based on advective transport of "water" particles and does not consider additional processes such as sorption, dispersion, and diffusion that would affect the travel times of a ground-water contaminant. Travel times also are directly related to assumptions about aquifer porosity. Since no measured values of porosity exist for the study area, the simulations use a uniform value of porosity for each layer as estimated from typical values for the lithologies of the layers. If porosity estimates are too high, travel times would be underestimated. If porosity estimates are too low, travel times would be overestimated.

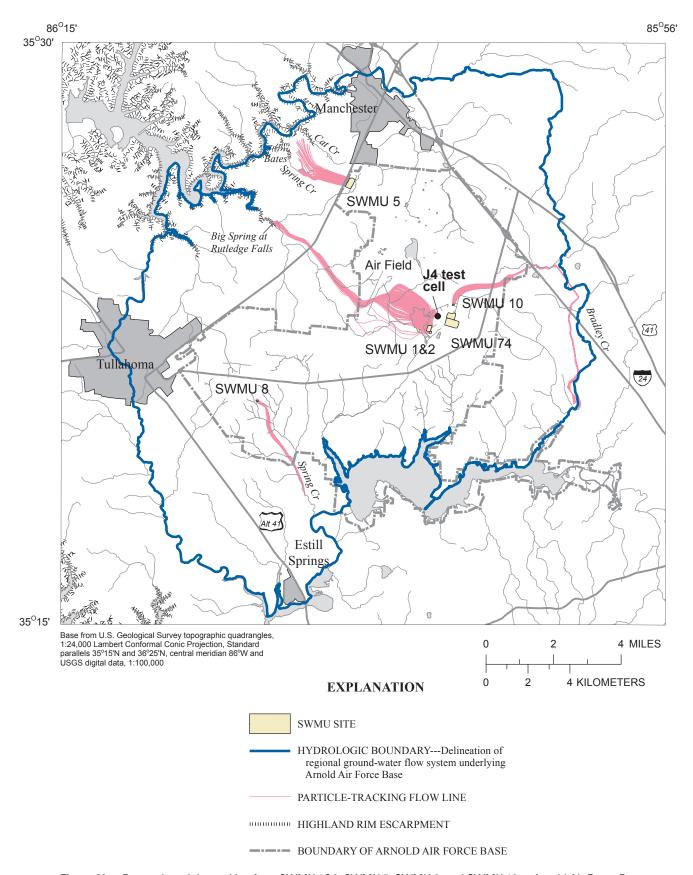


Figure 30. Forward particle tracking from SWMU 1&2, SWMU 5, SWMU 8, and SWMU 10 at Arnold Air Force Base with no ground-water withdrawal wells pumping.

Figure 31. Forward particle tracking from SWMU 10 at Arnold Air Force Base under an alternative calibration of the flow model.

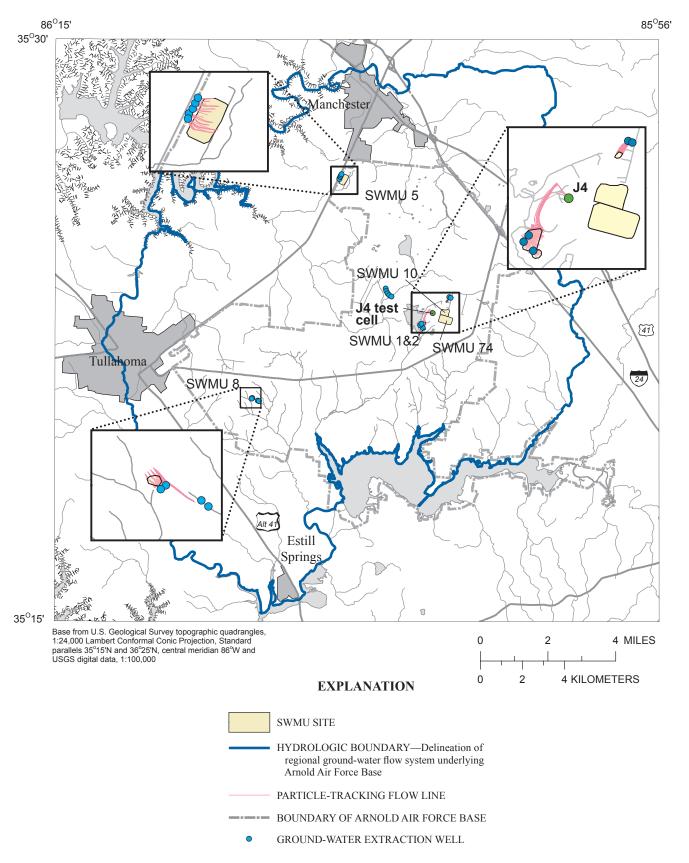


Figure 32. Forward particle tracking from SWMU 1&2, SWMU 5, SWMU 8, and SWMU 10 at Arnold Air Force Base with ground-water withdrawal wells pumping.

Figure 33. Forward particle tracking from SWMU 1&2 at Arnold Air Force Base with the airfield road ground-water withdrawal wells pumping.

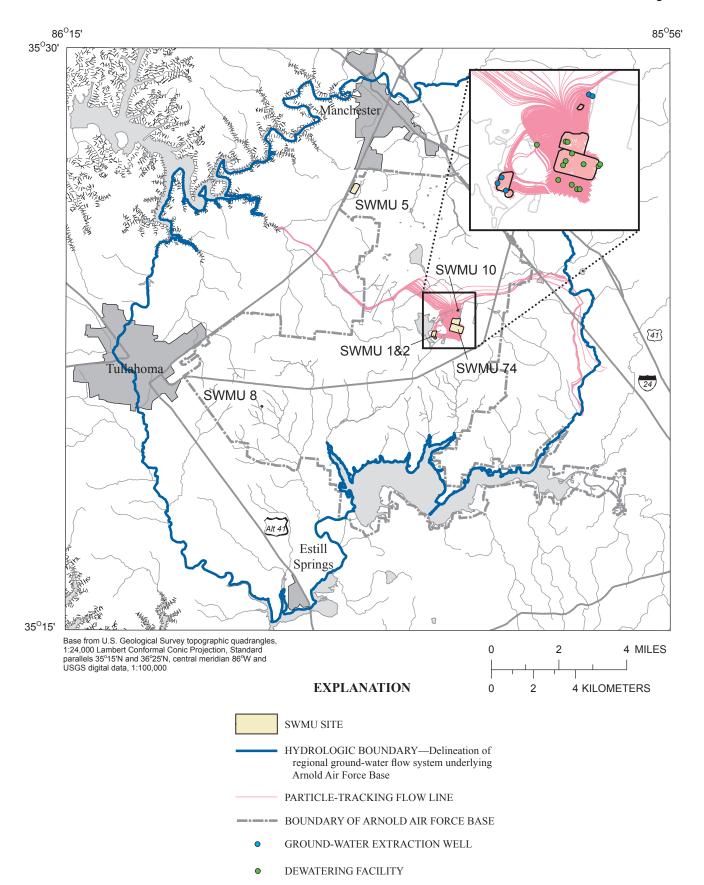


Figure 34. Forward particle tracking from the Main Test Area (SWMU 74) at Arnold Air Force Base with all dewatering facilities turned on.

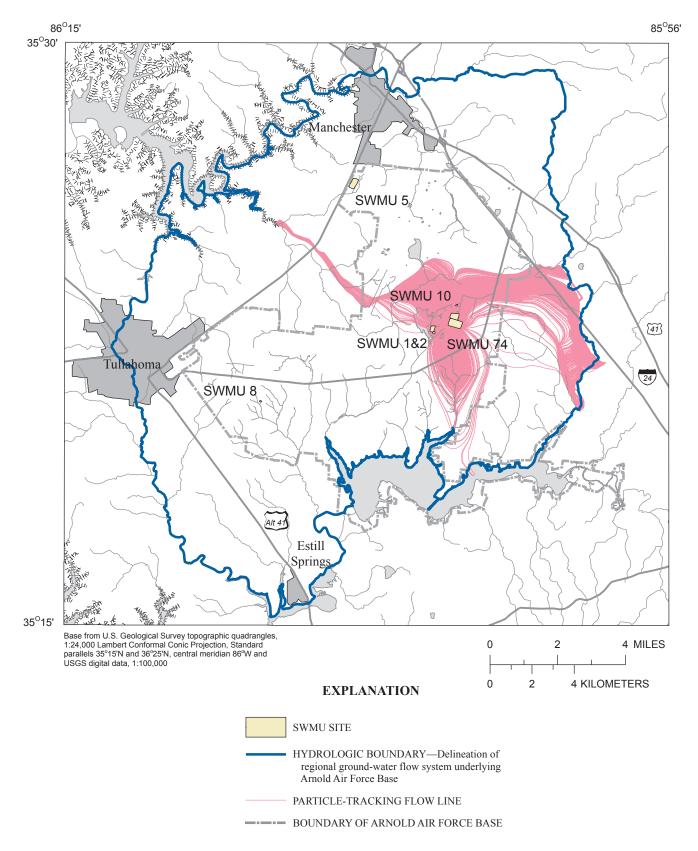


Figure 35. Forward particle tracking from the Main Test Area (SWMU 74) at Arnold Air Force Base with all dewatering facilities turned off.

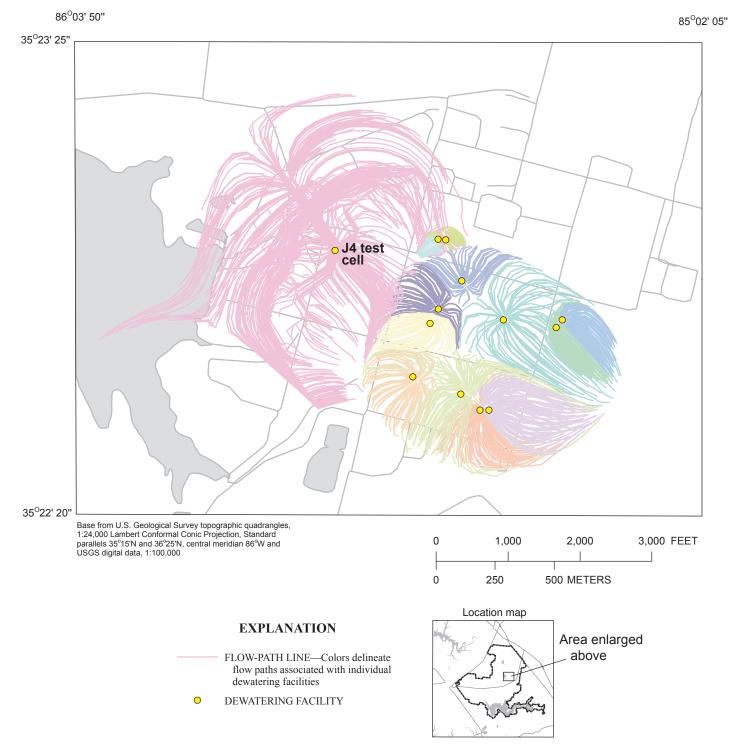


Figure 36. Backward particle tracking from dewatering facilities at the Main Test Area at Arnold Air Force Base.

Summary

Arnold Air Force Base (AAFB) occupies about 40,000 acres in Coffee and Franklin Counties, Tennessee. The primary mission of AAFB is to support the development of aerospace systems. Numerous site-specific ground-water contamination investigations have been conducted at designated Solid Waste Management Units (SWMUs) at AAFB. Several synthetic volatile organic compounds (VOCs), primarily chlorinated solvents, have been identified in the ground water at AAFB. Two ground-water contaminant plumes that originate at AAFB, the "SWMU 8 plume" and the "northwest plume," have been shown to extend to regional discharge points outside the AAFB boundary.

The ground-water system at AAFB can be divided into several different zones or aquifers. The Manchester aquifer, the primary source of drinking water in the area, consists of chert gravels at the base of the regolith and solution openings in the upper part of the bedrock. A ground-water divide, approximately coinciding with the Duck River-Elk River surface-water divide, underlies AAFB and extends from southwest to northeast. Ground water flows from the divide area to the discharge areas, which are the major streams, springs, lakes, and reservoirs around the base. Several troughs are present in the potentiometric surface. The most prominent trough trends northwest to southeast in the Crumpton Creek Basin. The troughs in the potentiometric surface are believed to be associated with zones of high permeability within the aquifer that are important regional flow paths. These pathways share the following characteristics: a depression or trough in the bedrock surface, a trough in the ground-water surface, low gradients in the ground-water surface, and a large spring or group of springs at the downgradient end.

In the study area, recharge occurs from direct infiltration of precipitation throughout the study area. Based on water-budget and stream base-flow data, the AAFB study area can be divided into four areas with different recharge rates. The areas are: The Barrens area along the regional drainage divide; the Spring Creek, Dry Creek (at Estill Springs), and Taylor Creek Basins in the southwestern part of the study area; Sinking Pond; and the rest of the study area.

Ground water is withdrawn at numerous locations at AAFB for two primary reasons: ground-water withdrawal wells associated with ground-water contamination and dewatering activities around below-grade testing facilities. Ground-water withdrawal wells currently (2005) are operating at SWMU 1&2, SWMU 5, SWMU 8, and SMWU 10. Dewatering activities also occur at more than 20 facilities at AEDC.

The previous ground-water flow model (1992) was updated to incorporate new data and concepts about the ground-water flow system. For the computer flow model, the Highland Rim aquifer system was divided into four layers to simulate ground-water flow. The layers were defined on the basis of differences in physical characteristics that affect hydrologic properties. Model layer 1 corresponds to the

shallow aquifer. Model layer 2 corresponds to the upper part of the Manchester aquifer. Model layer 3 corresponds to the lower part of the Manchester aquifer. Model layer 4 corresponds to the Fort Payne aquifer.

Model parameters (Harbaugh and others, 2000) were defined for recharge and hydraulic-conductivity zones. The digital model developed for this study was calibrated to steady-state conditions as defined by averaging measurements from spring and fall 2002. Overall, simulated water levels agree reasonably well with observed water levels. Water-level data at 615 wells were available for comparison to simulated conditions. The root mean square error for measured compared to simulated water levels was 9.8 feet. The average head difference between measured and simulated heads is -0.47 feet. The model has seven hydraulic-conductivity parameters with calibrated values that range from 0.2 to 6,500 feet per day. The model has four recharge parameters with calibrated rates of 4.2, 7.8, 17.7, and 110 inches per year (the high value represents focused recharge at Sinking Pond). The calibrated recharge rates correspond to an average recharge rate over the entire model area of 7.6 inches per year.

Particle-tracking flow paths were analyzed from selected SWMUs. From SWMU 1&2, most of the particles (70 percent) move to the northwest under the retention pond, then move west under the air field, then follow a prominent trough in the ground-water surface to discharge to Big Spring at Rutledge Falls. Pathlines from SWMU 5 show that particles generally move west and northwest to discharge to Cat Creek, Bates Spring Branch, or seeps and springs along the Highland Rim escarpment. Pathlines from SWMU 8 show that particles move to the southeast to discharge along Spring Creek. Pathlines from SWMU 10 show that particles move to the northeast before turning south to discharge to springs along the lower reach of Bradley Creek. Under an alternate calibration of the flow model, particles from SWMU 10 diverged to show two flow paths that both discharged to springs along the lower reach of Bradley Creek. Based on a detailed review of local water levels and water-quality data, this alternate scenario is believed to be less likely than the first one presented here, but may occur periodically or seasonally.

Currently (2005), ground-water withdrawal wells are operating at SWMU 1&2, SWMU 5, SWMU 8, and SWMU 10. Particle-tracking results from these SWMUs, under conditions with the ground-water withdrawal wells pumping, show that no particles leave the SWMUs. In 2005, five new ground-water withdrawal wells along the airfield road were scheduled to begin pumping to capture ground-water contamination that has already migrated beyond the SWMU 1&2 boundaries. The airfield road ground-water withdrawal wells and the J4 test cell capture about 89 percent of the particles from SWMU 1&2. About 11 percent of the particles under this simulation discharge near Rutledge Falls.

Three particle-tracking simulations were run to analyze the effects of dewatering facilities on flow paths in the Main Test Area (MTA). These simulations illustrate that the dewatering facilities have a substantial effect on flow paths

from the MTA and are effective in containing most of the ground water in this area.

The updated ground-water flow model is consistent with all current data on the ground-water system at AAFB. The model should provide a reliable tool to assist AAFB in managing the ground-water resources at the base.

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